Louisiana DOTD Experience with CPT for Driven Pile Design

> Mark J. Morvant, P.E. Louisiana Transportation Research Center



Louisiana CPT Systems





Twenty-ton truck

- LTRC Research
- DOTD Production
 220' max depth

Minicone truck LTRC - Research 40' max depth



Available Cross-sectional area: 2 cm² Cones: • Friction MINICONE • Piezo 60 degree cone tips Available Cross-sectional area: 10 cm² Cones: **BIG CONE** •Friction Piezo Cross-sectional area: 15 cm² Ceramic •Single, U2 stone allows U2 •Dual, U1 & U3 U3 Located at porewater to Location, if •Seismic end of sleeve, enter, U1 available If available •Conductivity

CPT Technology In Louisiana

Primary Uses

Load carrying capacity of piles

 end-bearing piles (mid 80's to present)
 friction piles (2000 to present)

 Soil classification (stratification)
 Soil improvement (relative density)

Current Research Effort Consolidation parameters Subgrade Resilient modulus (mini-cone)



CPT Experience for Driven Piles End-bearing Piles : Locating dense sand layers

Precast Concrete Piles Timber Piles Steel Pipe Piles



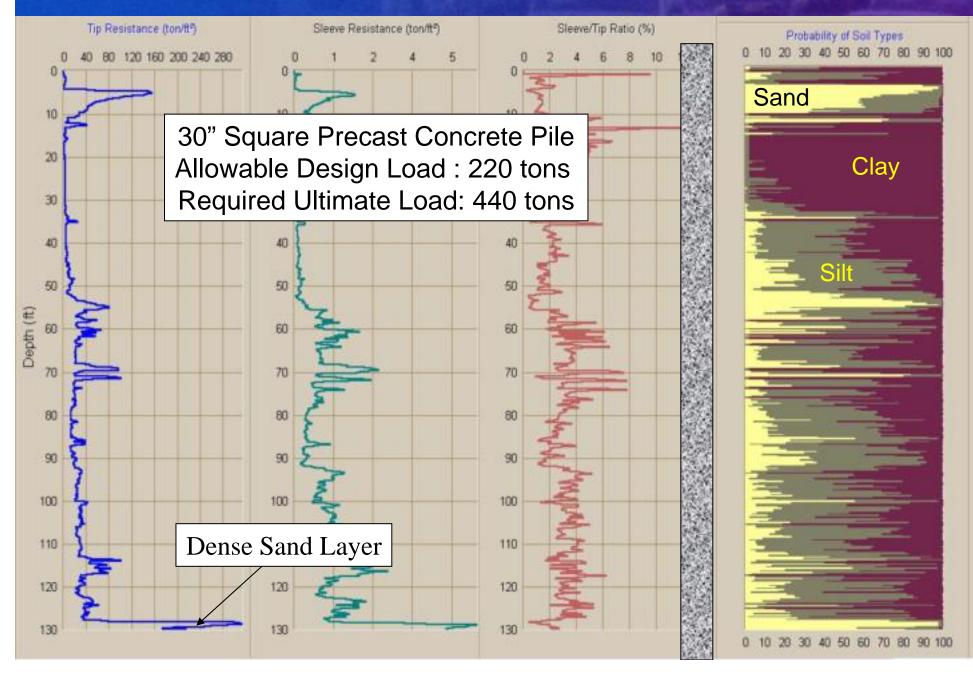
I-310 New Orleans

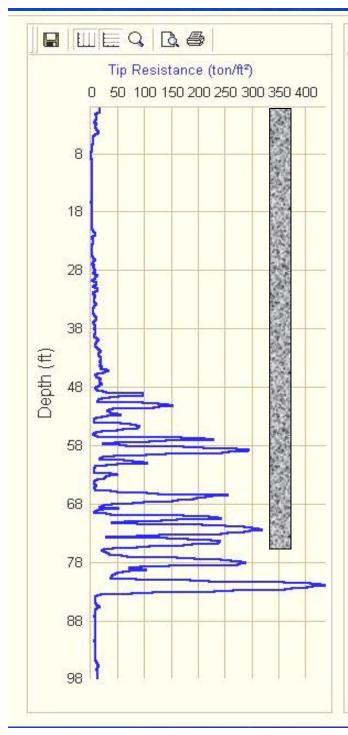


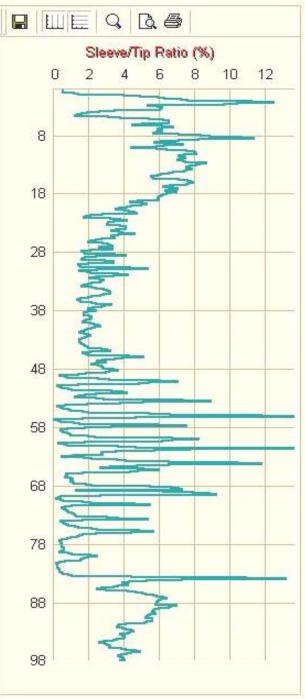
Acceptable blow count based on CPT

Overdriving based on boring

Typical South Louisiana CPT log







	Soil Types - Robertson'86
/. Stiff	Clay with layers of Sand
Clay w	ith layers of Stiff Clayey Sand
Clay	
Stiff CI	ayey Sand and Clay
Stiff CI	ayey Sand with layers of Silt Sand
Stiff CI	ayey Sand with layers of Sand
Stiff CI	ayey Sand with layers of Sand
Stiff CI	ayey Sand with layers of Silt Sand
Stiff CI	ayey Sand with layers of Sand
Sand t	o Clayey Sand
Stiff CI	ayey Sand and Gravel
V. Stiff	Clay and Gravel
Gravel	with layers of V. Stiff Clay
Gravel	y Sand to Sand
Gravel	with layers of Stiff Clayey Sand
	Clay with layers of Stiff Clayey Sand

LTRC Research Project

Evaluation of Bearing Capacity of Piles From Cone Penetration Test Data 1998

Principal Investigator: Hani Titi, Ph.D, P.E. Co-Principal Investigator: Murad Abufarsakh, Ph.D., P.E. Project Manager: Mark Morvant, P.E.



DOTD Test Piles

- Precast concrete piles with CPT data
 - 60 piles identified

- Test loaded to failure
 - 40 piles identified
- Skin friction is the major component
 - 34 piles analyzed
- Implementation Phase (2001)
 - 17 piles added to database
 - Total 51 test piles analyzed

Load Capacity Methods

- Load Test Results
- Traditional Static Analysis
 - Alpha method (Tomlinson)

CPT Methods:

- Schmertmann
- de Ruiter and Beringen
- Bustamante and Gianeselli (LCPC/LCP)
- Tumay and Fakhroo
- Aoki and De Alencar
- Philipponnat
- Price and Wardle
- Penpile

SOIL CLASSIFICATION Soil-CPT Program

STATISTICAL APPROACH

1. Zhang, Z., and Tumay, M.T., "Statistical to Fuzzy Approach Toward CPT Soil Classification", JGE, ASCE, Vol. 125, No. 3, <u>1999.</u>

EXPERIMENTAL APPROACH

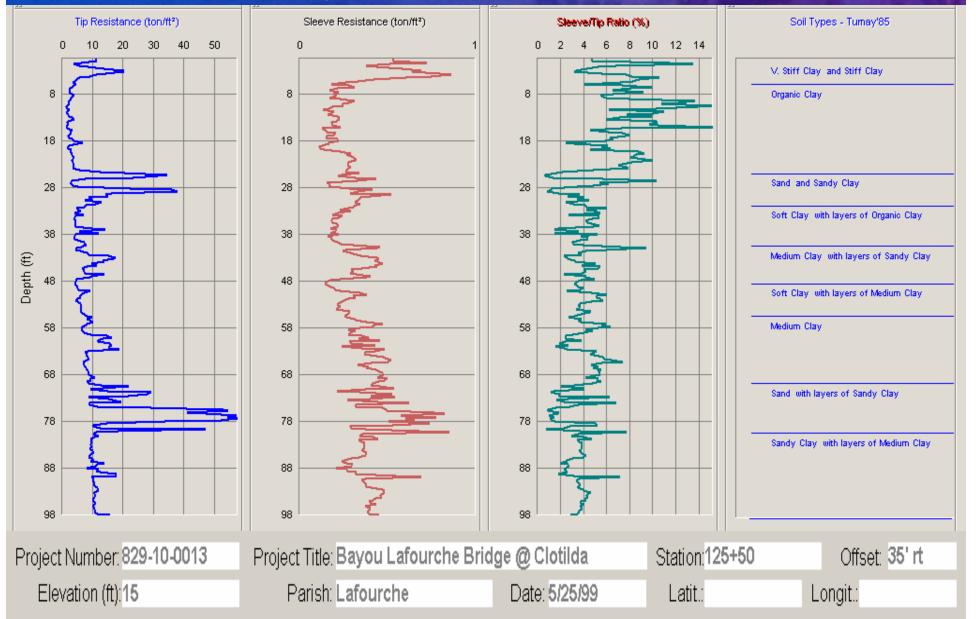
2. Tumay, M., Report No. FHWA/LA/LSU-GE85-02, LTRC, 1985

3. Robertson, P.K., Campanella, R.G., Gillespie, D., and Greig, J., "Use of Piezometer Cone Data", ASCE, <u>1986</u>



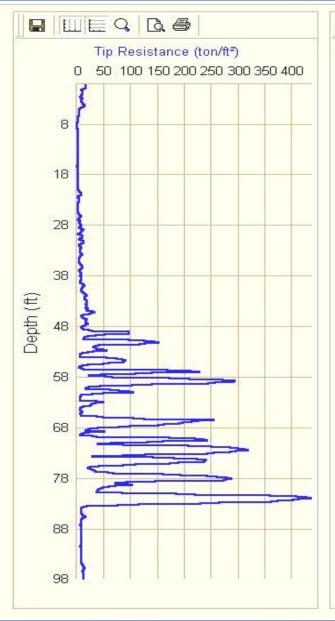
Soil Classification: General Soil Type

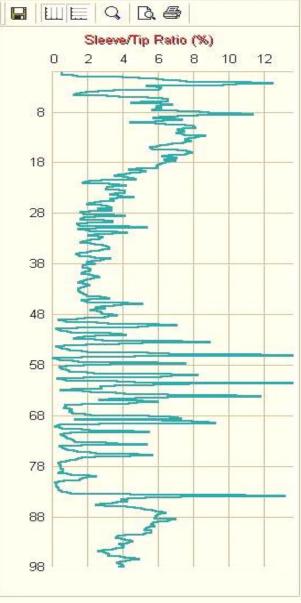
Tumay, M.T (Modified Schmertmann)



Soil Classification: General Soil Type

Robertson (no pore pressure)



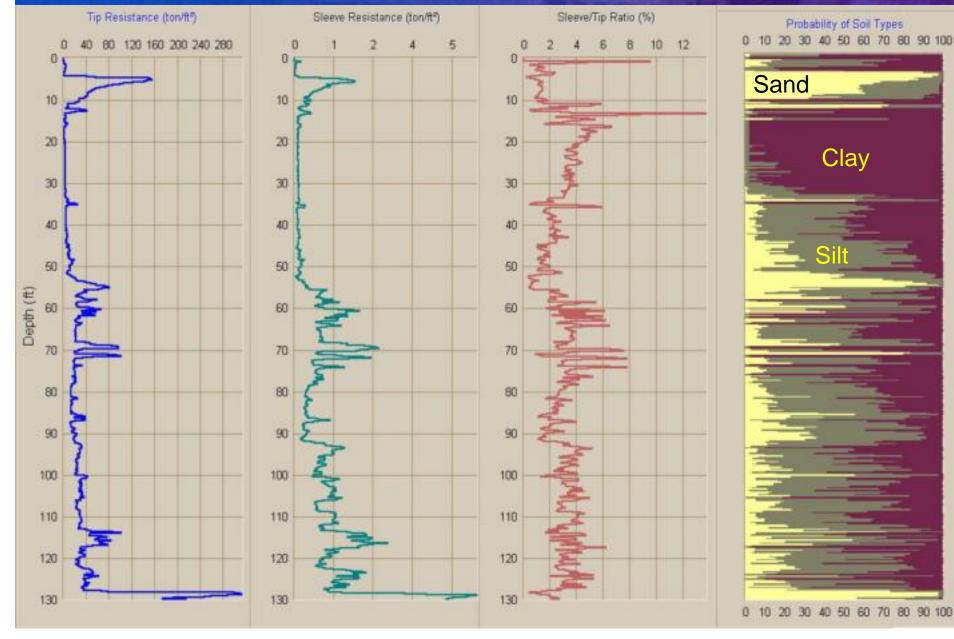


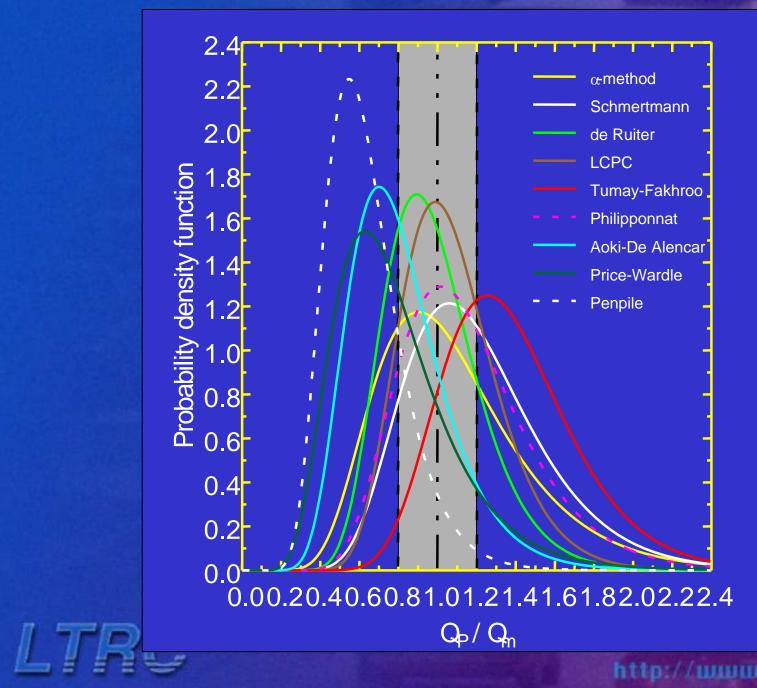
D.	8		
	0.0	 Datas	3

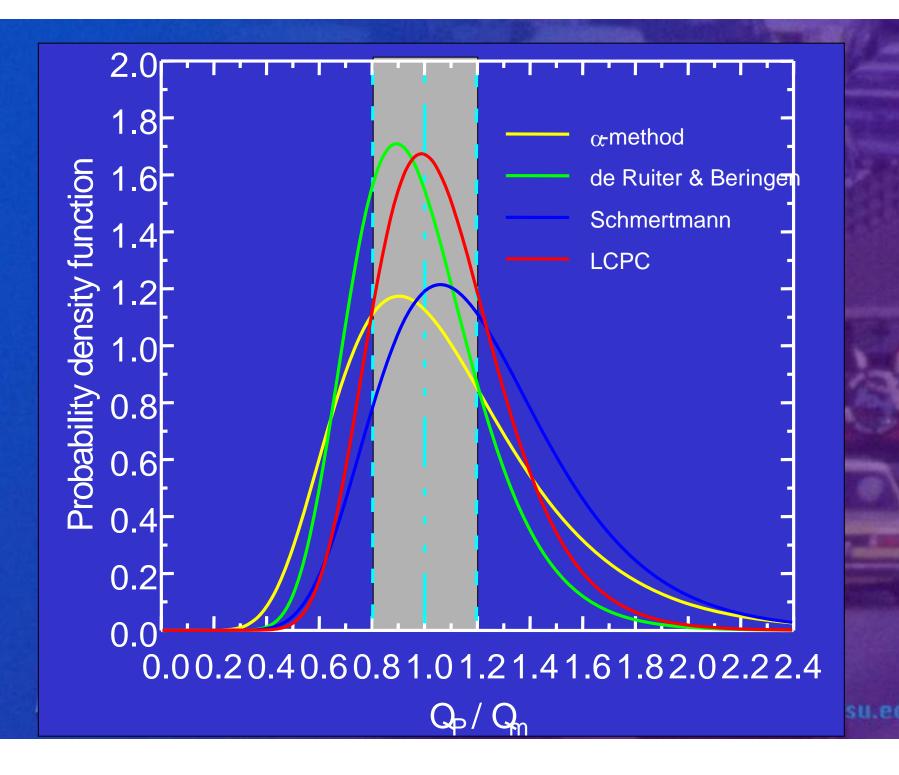
v. Stin (Clay with layers of Sand
Clay wi	th layers of Stiff Clayey Sand
Clay	
Stiff CI:	ayey Sand and Clay
Stiff Cla	ayey Sand with layers of Silt Sand
Stiff Cla	ayey Sand with layers of Sand
Stiff Cla	ayey Sand with layers of Sand
Stiff Cla	ayey Sand with layers of Silt Sand
Stiff Cla	ayey Sand with layers of Sand
	o Clayey Sand
V. Stiff (Clay and Gravel
Gravel	with layers of V. Stiff Clay
Gravely	/ Sand to Sand
Gravel	with layers of Stiff Clayey Sand
. over	Clay with layers of Stiff Clayey Sand

Soil Classification: Statistical Method

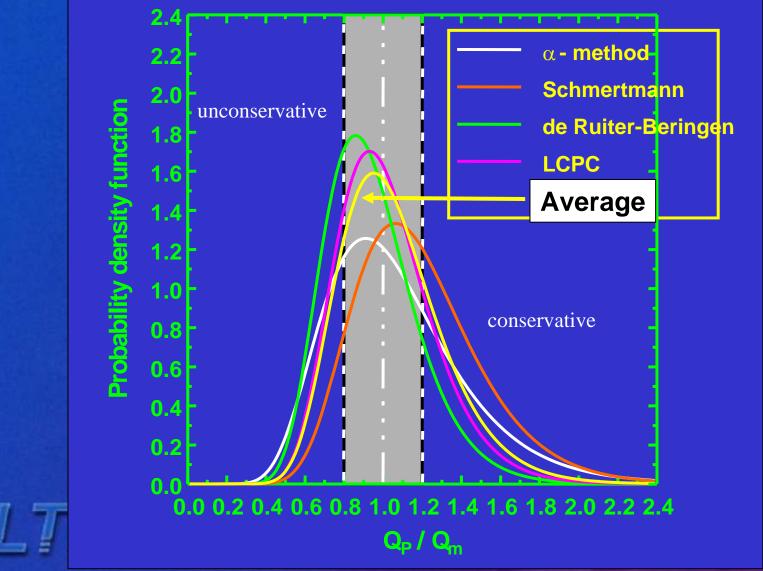
Zhang, Z., and Tumay, M.T





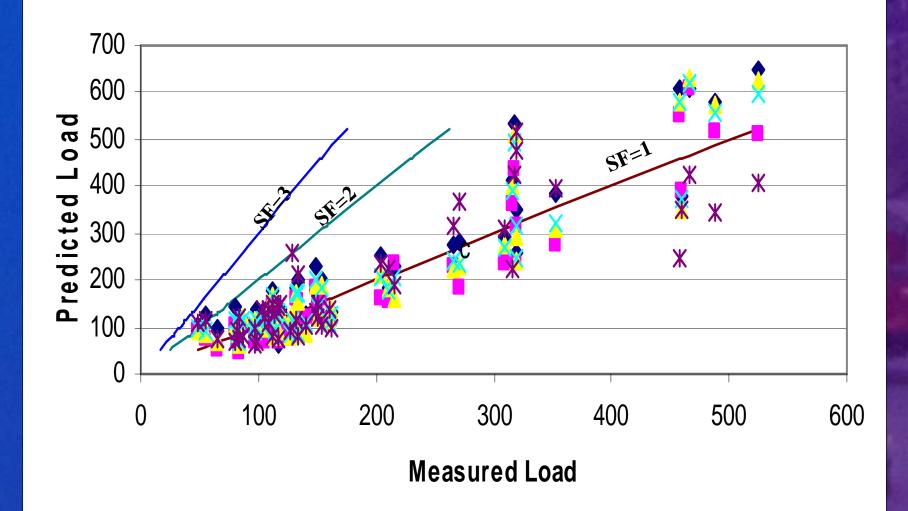


Statistical Analysis: Including Average of Methods



rc.lsu.edu

◆ Schmertman ■ deRueter ▲ LCPC × Ave ★ Alpha





DOTD Design Policy for Piles

 AASHTO Design Codes WSD (foundations) LFD (structures) LRFD (proposed)

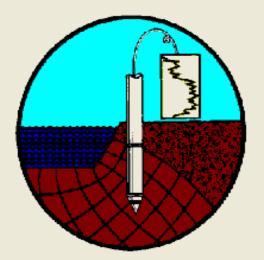
Safety Factor on Load Capacity (WSD)
 3.0 without test piles
 2.0 with test pile verification

 Current Policy: CPT for Design CPT included into bid plans Plan length determined by CPT Average of Methods Boring Data Correlation Test Pile Correlation

Pile Design Program

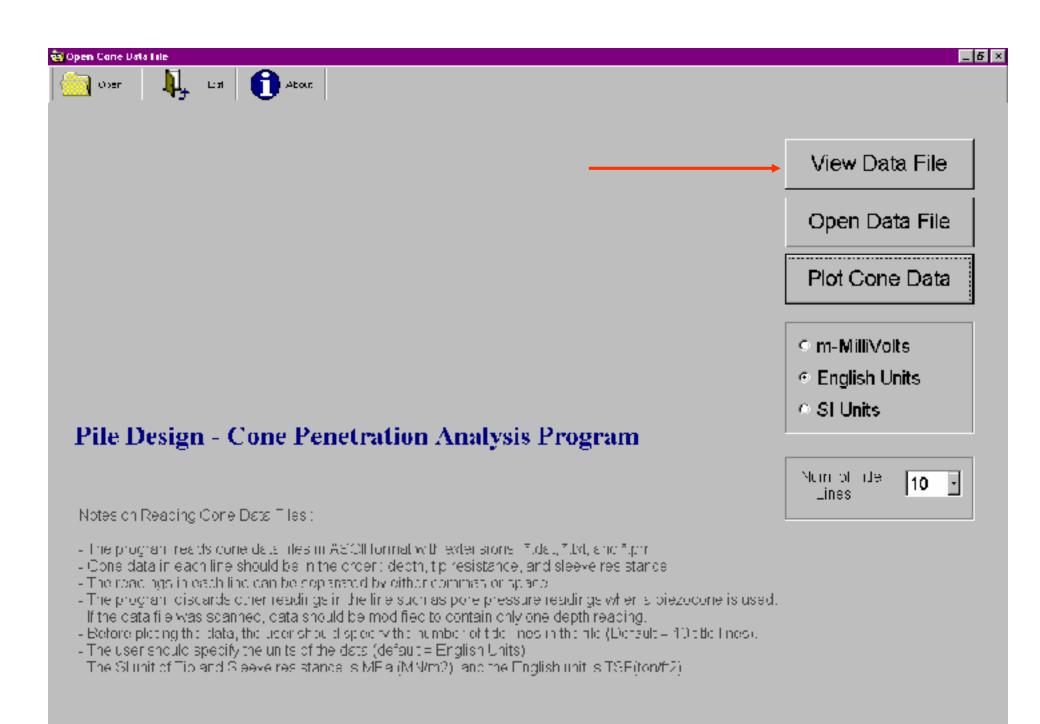
Louisiana Transportation Research Center

LOUISIANA PILE DESIGN by CONE PENETRATION TEST PROGRAM

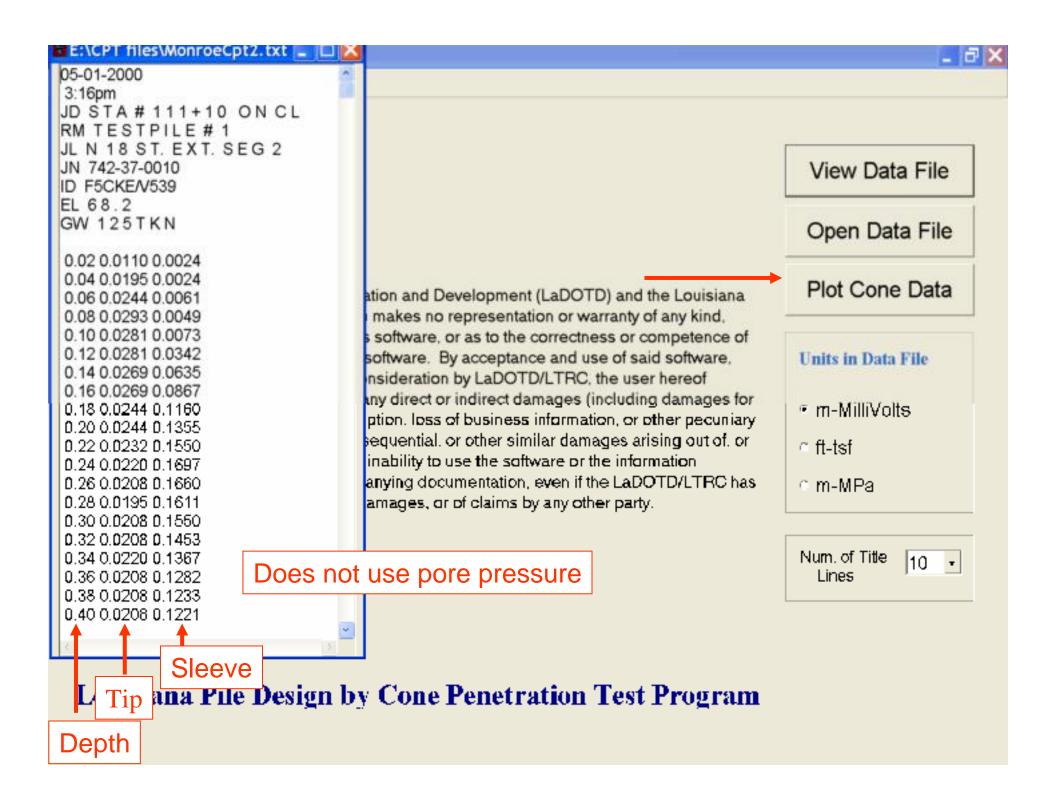


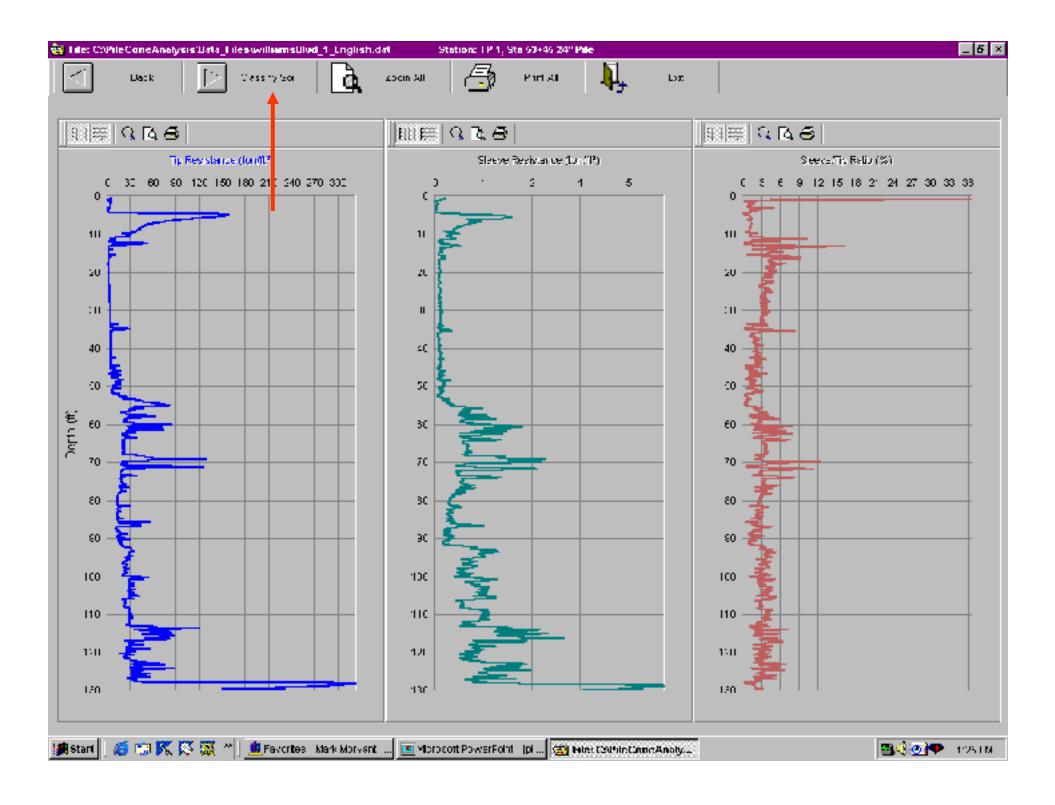
Version 2.3

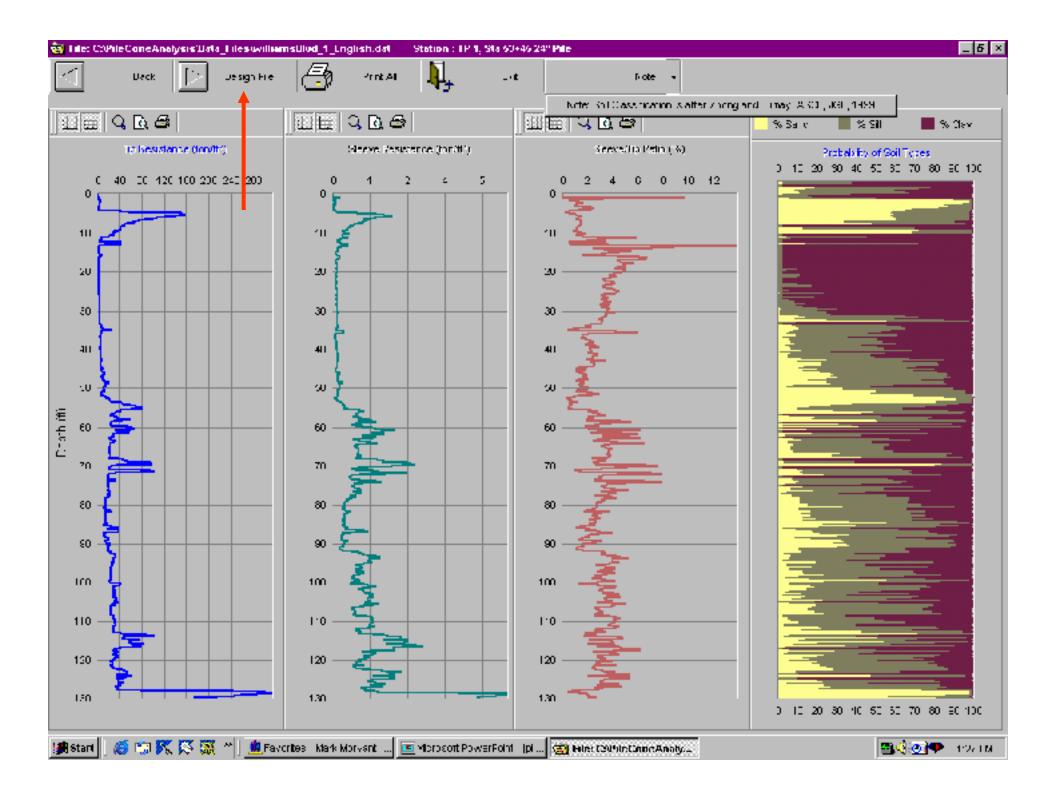
Available for download: www.ltrc.lsu.edu

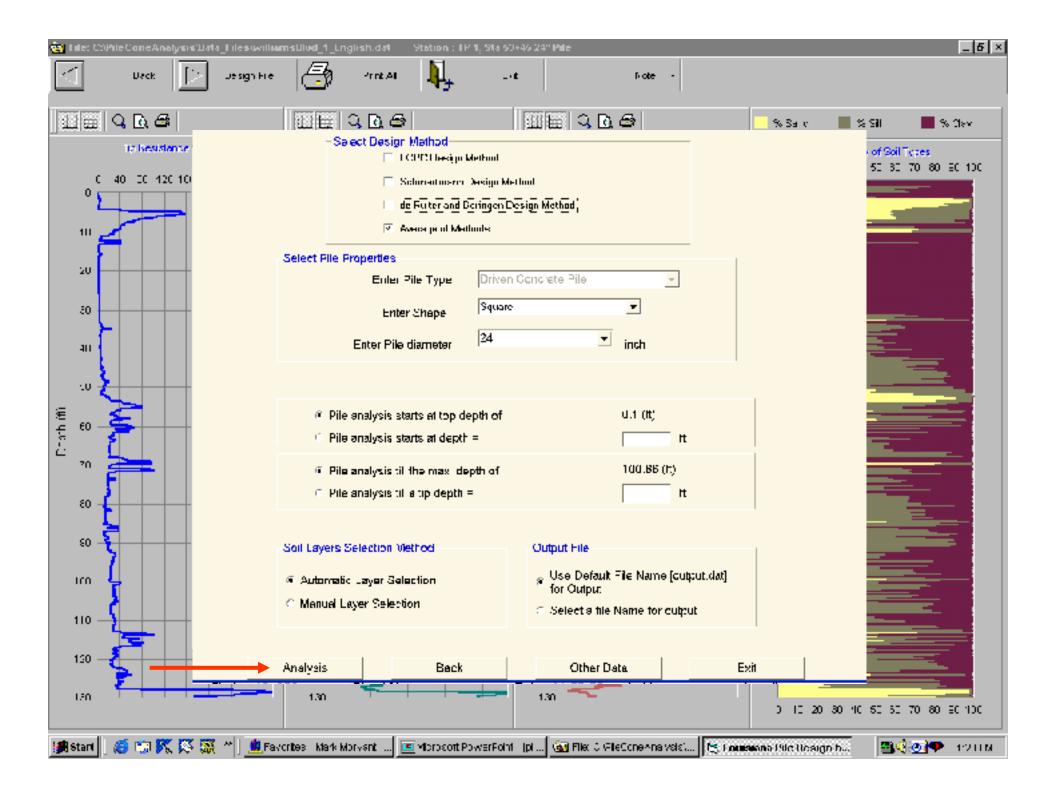


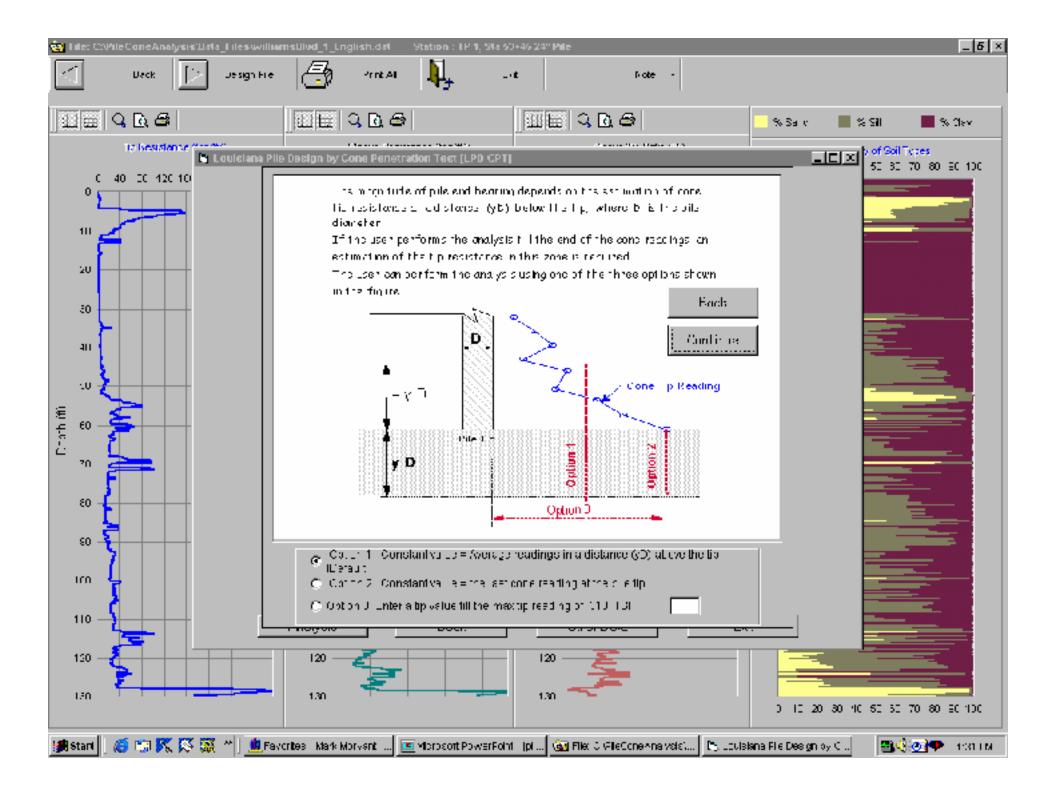




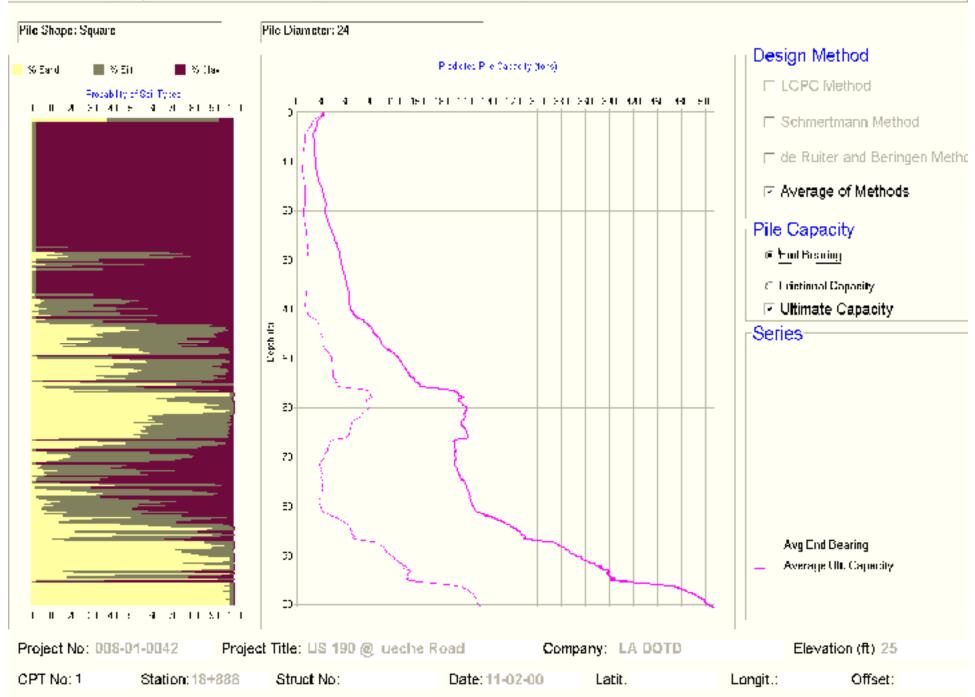








Back 🗖 Depth / Elevadors - Correction Factor 🖉 🛛 Print 🕠 🛛 Exit



Ξ.

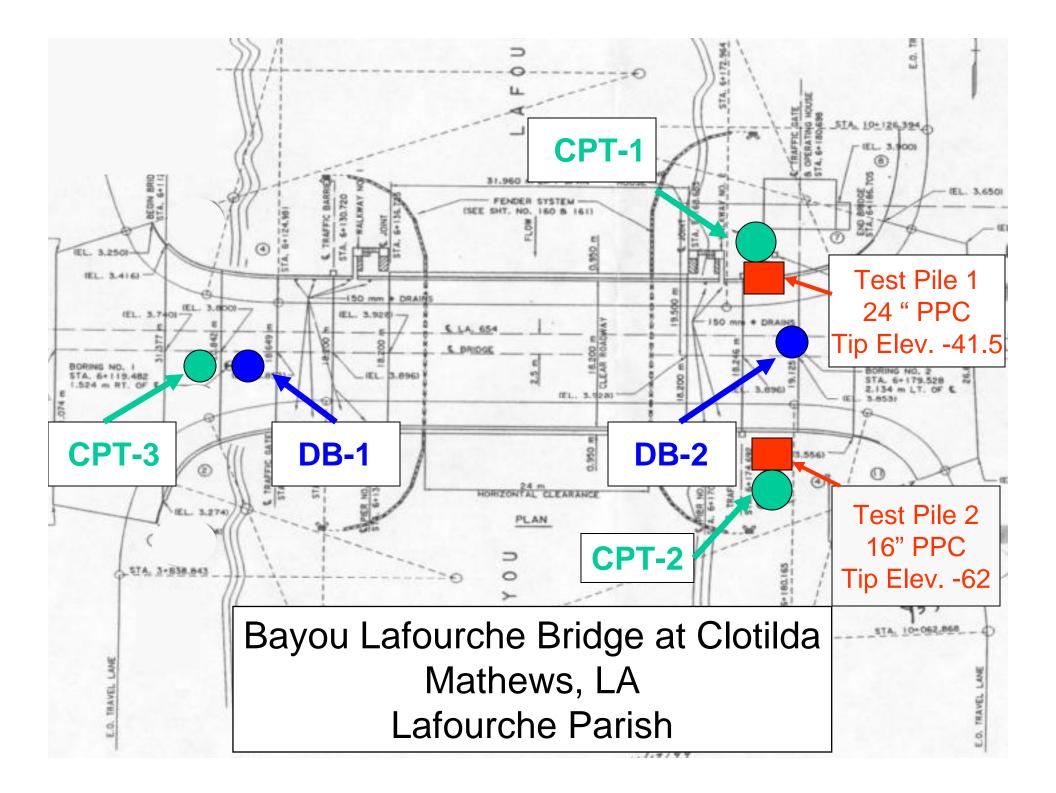
Bayou Lafourche Bridge at Clotilda Mathews, LA Lafourche Parish

Foundation: Required Load: Tip Elevation: Load Results: 24 " Test Pile 105.6 Tons -41.5 66 Tons 16" Test Pile 102.2 Tons -62.2 > 154 Tons (Did not fail)

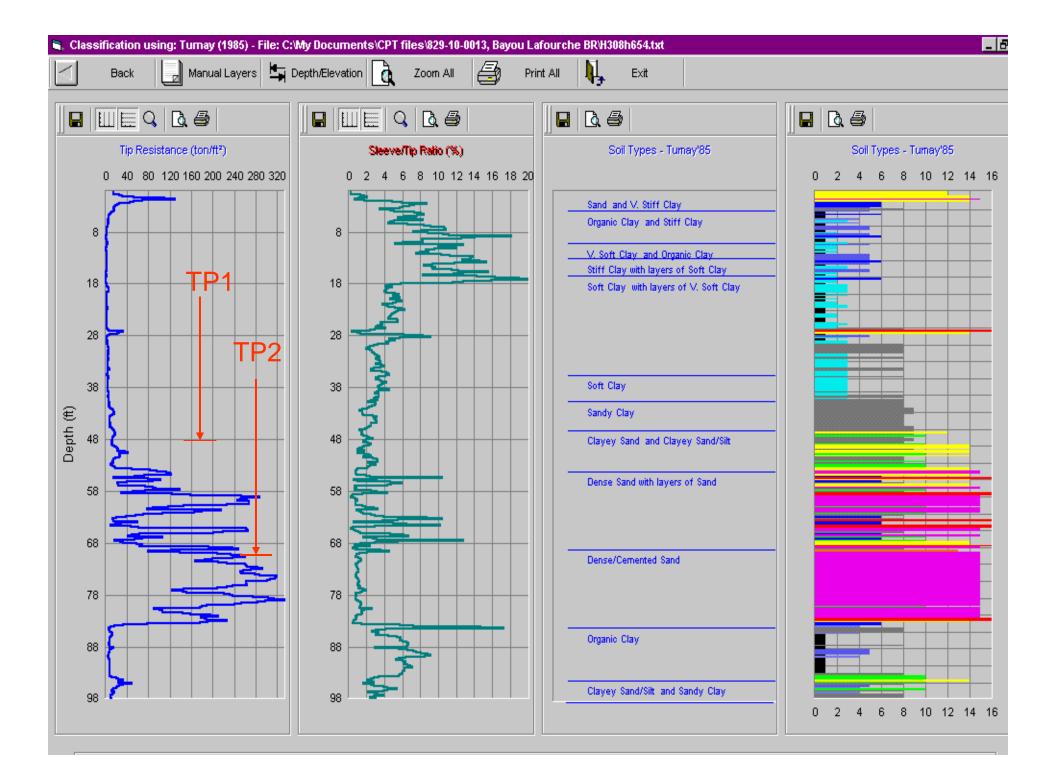
CPT Application:

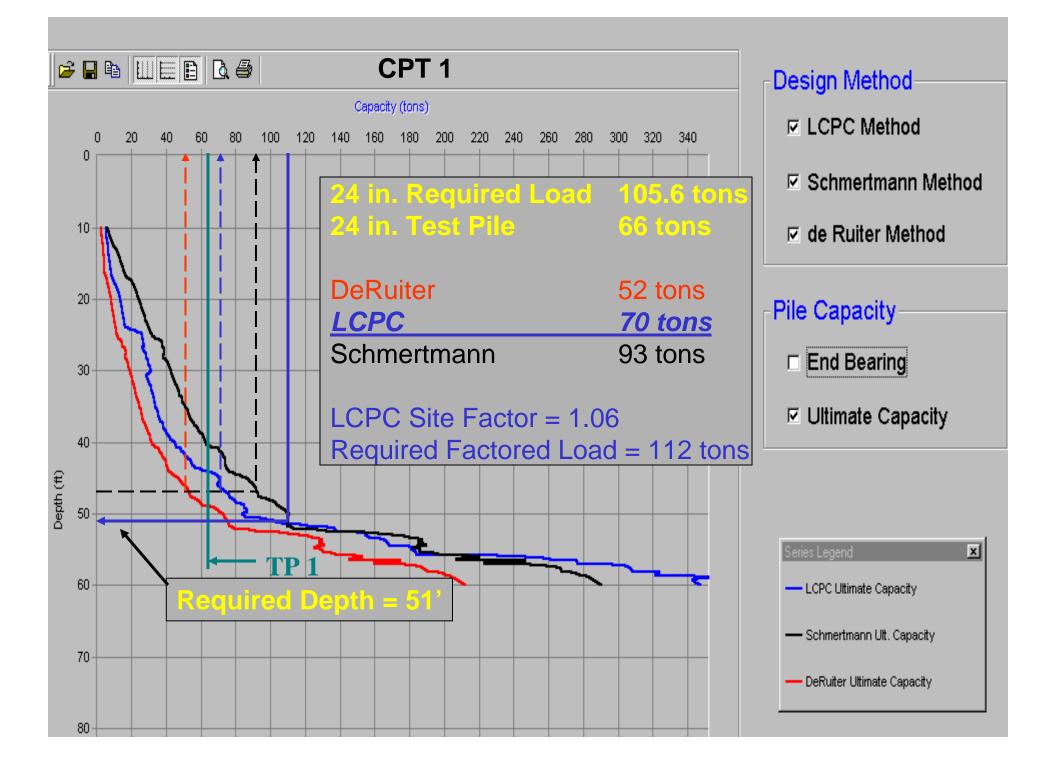
Correlate with load test to determine pile order lengths

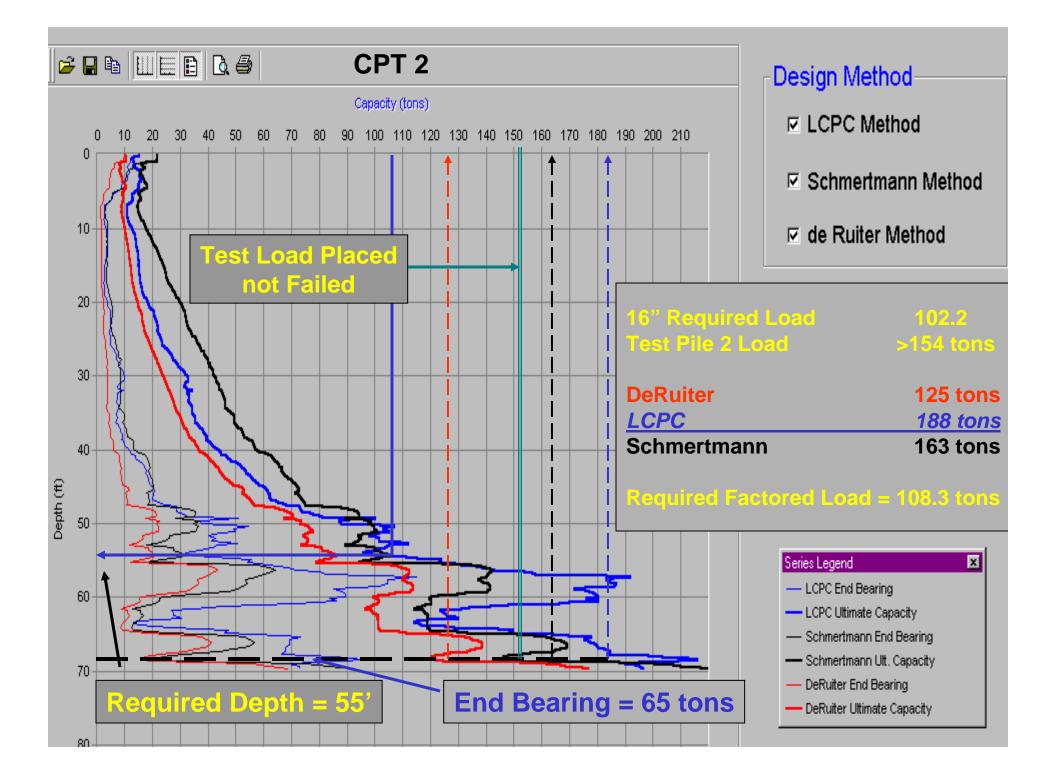


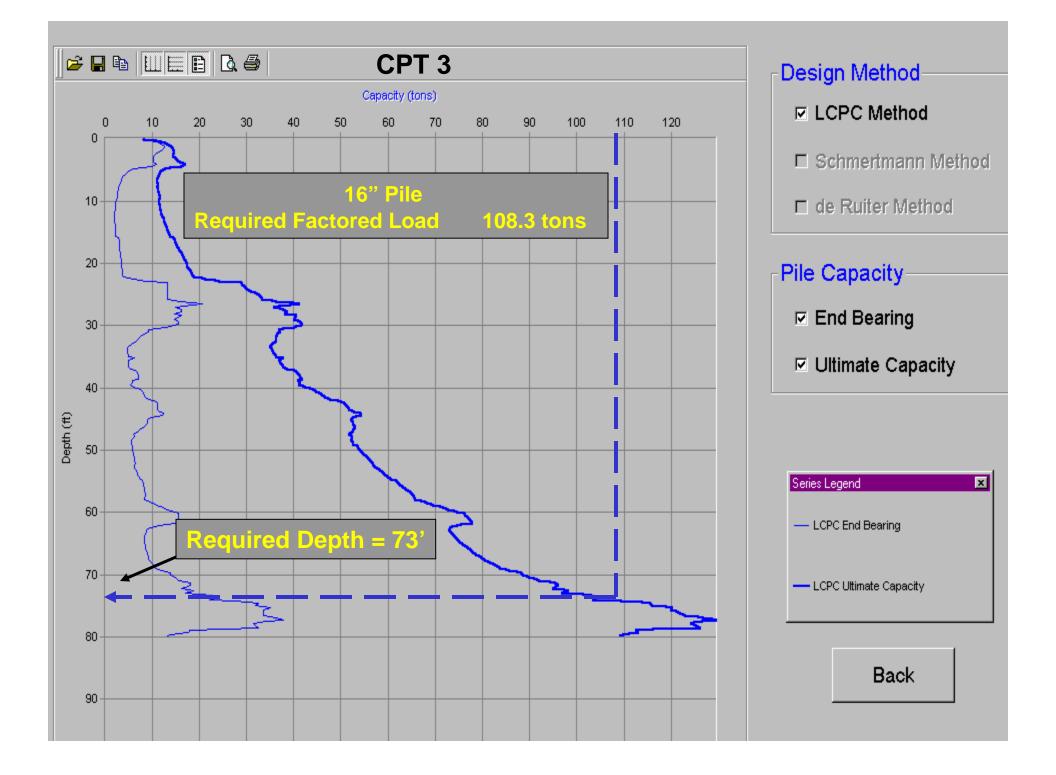


8. 34. 47a	115	88		12 4	- 5 6-)		y Con I			1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	1.000			122	-	30	5		-	H.8	ഖ	1.3
	114	6	-	13. 0	1.55		+-a¶	20)	<u>*</u>				CE LIDAL CL.	in	-	32	2	0.17	-	YLD.	١	10
	118		25	11		11	M. 3.	Ð	5					120	-	36		-	_	M.S.		
35. 3	10	-	23	4				ы		a second					-						_	112
CHERTIC BL. WY						_	-	_	20	1.			WITE SA. 686.181		28	5		0.43			ରୁ	1
. ciić.	100	22	56		6.72			포	-	La En	13.5		WTR.SA. 088.175	n	28	40	15	0.57		¥D.	0	20
2.CL. +172.075.	ien (43	54-)	21 p	<u>672</u>		ЧЧФ.	Θ	25	the second se	1.0		MTR. 34. 4 olds.	in	34	37	0	6.47		yes	Ð	
0.51.554	11%	-	м.	P.		÷.,	4.0.	ତା		355	1.00		GR.CL. WITE SA. I'R.	113	34	67	38	OA2	_	3)3	1	25
	115		H.	P. 1			M-5	ଚ	30	State of the second	1.7.1		. LIXA CL. MITE.	114	47	47	20	0.43			õ	
WARA. I TE DES.	112	-	-	13	مند. ه	- 1		ର୍ଭା	-14	1	1.0		ST 10 . 43 18 95	117					_	_	_	30
WINK BA. 1 CBG.		-	-		_				35	State File	1000				-	ы.	P.				ଭ	
12. 14. TF. 31	63	37	21	-12	0.5%			51		S				117	-	44	Ko				9	35
	SD	51 j	m)	24	0.90		φæ,	6	40	11.35 64.77	1.397		AT. MIL. CH. CL. WIT	11.2	98	85	14	2.1K		H.S.	9	۱.
BLASTIC SL.		64	63	4	o:⊐#		210				3.6.33		CE. SA. SI	124	-	24	1				õ	1-00
5.54.51.94	122	_	н.	•		644	H.3	65	45	A CONTRACTOR OF THE OWNER OF THE	1. 1. 1. 1.		WITE ORG.	124	-	31	-	-	1.42	10.0		1
T. STE GE SA. W	_		_	P.		1.14		_			1997.68			1.40	-	31	6		_	The	ଭ	1-1-2
		_	N.					G	<u>30</u>		1.1.1.1			120	-	23	1			H.A	ତ	
CE. LEAN CL	ملائد	. 45 .	ടാ	- 10	0 40			_	-201		1		00.01		-		_	-		-		150
P. C W172.0785.	112	-10	74	42	1.18		345	ତା	55		14		WITE SA.	115		63	32				0	1
-		_				<u> </u>			50	TP 1	120					-		-	-	-	-	5
WITE. ORG. K	111	-13	ms	4 7	28.0		-1-	ତା	60				WITE ORG.	-	57	100	5	244		ala	9	
EM			<u> </u>			-		_	60		4.00				-	-		~ ~ ~	_		-	60
2. 51. MSA . + 12.	121	—	FA .	P.				\odot	65		Secons		ALT. STE. SR. CL.	2	m	8-	56	0.12		YUD.	9	1
54.				<u> </u>			-		100		500		GR. SA		-	N.	P.	_		_	-	6
2. CL. WATE OFF.	່າເອັ	45	177	-5	ъ. ið		20	5	\mathbf{p}				ALT. STR. CR. C. W		-	21	34				0	
					-				-04				GR. MA.		-	н.	P.	_		_	-	170
P. SA.SI. MTR.	118	_	64.	P. J	6	1.0	m.a.	\odot	75	_		_	WITE SH.								3	L
PC	<u> </u>			· · · ·		<u> </u>			12	-	TP 2	2	with an.		C	SP.	ТΙ	<u>ا ا</u>	_ 1	0	-	1.75
72.04.		at	83		0.85	i	30	ତ				<u> </u>	WITE SH.				11	N =	= 1	U		
G2.81.				18	-		-		80				WITE. On.				-	-		_		80
P. TLASTIC SI.	100	(ទេ)	ا عالا إ	1 m	1			6	and .				GR. SA. SA. WICL .			36	13				8	
			1			1		-	85				TP. SH.		-	30	13				•	85
WITE.OFG.tsk	110	44	-	44	1.01	Ł		ତ	.				OP. CL.	115	45	86	51	1.53		ale	5	
W112.080.000	1		1	-	1	1	1	-	20				WITE ORD.	1.12				1.33		96		2
	1	jæ∖.	i		1.24		H-3.		I						-							
MTR.OFG.10H.			<u> </u>	1-			1		25				WITE OBS.	110	1	-	-	1.20		de		95
52. LLASTIC SI. WITE. 035.	02	51	63	45	1.34	3	313	6					WITE OEG.	-	57		1.1	1.34				
WITE. CHEN.	L~~		1~~	<u> </u>	1	1	1010									-	-	1.34		2/2	_	100
WAR 1876 . 4 West . wes	35	173	77	33	pA1	1	-	 ©					ALT. STR. GR. CL.		-	62	34	1			9	
A41-04-1.4001-440	1.0	L	l	<u> </u>			(-	100				SI. WISA.		-	ы.	P.			_	9	10
SP. CL. WATE DE	lun.	42	45	200	1.45	:	315	6									P.				9	
-		_		_		-			100				W/TR. 3A		-	ы.	F .			_	0	110
62.54.	118	1_	32	15	Ι.		м.5							1.70					1.68		6	
WHT2, 54, 1 12.		<u> </u>	<u> </u>		<u> </u>			-	115				MTR. SA.	120	-	41	17		-	<u> </u>	9	115
	1	I 1	١	. P.			1	6	1 1				GR. CL. MTR. ORG.	102	+5	74	40	1.18		ele	6	
WITE . 84 .	<u>i</u>		1 12		-	<u> </u>			121.21						_						-	1 120
E.C. WITE OBS.	104	6.0	82		1.25	-	0,0	154					GP. SI. M.SA.		-	н.	P.				\odot	
A.S. MOA. STRONG	115	-	н.	P		_		150	1:50				CR. BLASHIC SI.	107	1	75	40	1.65		212	88	134
ELANDE BL. MITE. W	100	16L	1.5	27	-	+	-	ŢΩ						110	4n	-	-	1.81		33	-	
TTE. SA.	1.	-		*	1.21		10125	160	HC				ANTE OBS.	100	57	68	28	1.90		ala		
THE REAL PROPERTY AND	103	121	-		صد		jala	- حوا					WITE	71	45	56	14	1.62		2/2	6	
THE REAL PROPERTY AND	1.04	•	100	47	2.13	1	313	le.	1150					101	50	34	7	1.51		cle	62	150
NOTE: LO HULHER TH						1							LO TT LOUT THAN									
February sootens r	4-1						1		1				LA. 308		-		5.3	1		1.10		
																						_









CPT vs. Conventional Drilling Method Deep Foundations

	Conventional Soil Exploration	CPT
Manpower	Crew: 4-5	Crew: 2-4
Time	Field: 6-8 / week Lab: 2-4 weeks	6-8 / day
Equipment	Drilling rig 3 support vehicles Lab equipment	CPT truck 1 support vehicle

CPT vs. Conventional Drilling Method (1998)

	Typical	Cost	
	Conventional Soil Exploration	СРТ	
DOTD	\$45/ft - \$50/ft	\$14/ft	
Consultant	\$50/ft - \$60/ft	\$28/ft	



CPT Benefits

Cost Savings

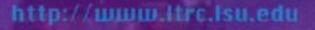
- Field exploration costs savings
- Laboratory costs savings
- Time Savings

Better subsurface stratification

- Finer Detail
- More locations

Accuracy

- Reduced number of test piles
- Shorter pile lengths



Questions?

